#### The Adjoint method in design

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## Discrete Adjoint method

Primal

$$\begin{aligned} & \mathsf{min}/\mathsf{max}/\mathsf{find} & & \mathbf{h}^T\mathbf{u} \\ & \mathsf{s.t.} & & \mathbf{A}\mathbf{u} = \mathbf{f} \end{aligned}$$

• Dual (Adjoint)

$$\begin{aligned} \min / \max / \mathrm{find} \quad \mathbf{f}^T \mathbf{v} \\ \mathrm{s.t.} \quad \mathbf{A}^T \mathbf{v} &= \mathbf{h} \end{aligned}$$

• If  $\mathbf{f} \in \{\mathbf{f}_i|i=1\dots p\}$  and  $\mathbf{h} \in \{\mathbf{h}_j|j=1\dots m\}$ , dual is cheaper when  $m \ll p$ 

#### Green's function interpretation

 $\bullet$  The Green's functions  $\mathbf{g}_A^{(k)}$  of  $\mathbf{A}$  are given by

A 
$$\mathbf{g}_A^{(k)} = \pmb{\delta}^{(k)}$$
  $k = 1 \dots N$ 

• Given the adjoint form

$$\mathbf{A}^T \mathbf{v} = \mathbf{h}$$

by strong duality,

$$\mathbf{v}^T \boldsymbol{\delta}^{(k)} = v_k = \mathbf{h}^T \mathbf{g}_A^{(k)}$$

#### Discretized design problem

Consider the following setting

$$\label{eq:continuity} \begin{split} \min_{\alpha} \quad J(\mathbf{U}, \pmb{\alpha}) \\ \text{s.t.} \quad \mathbf{N}(\mathbf{U}, \pmb{\alpha}) = 0 \end{split}$$

where

lpha : Design Variables

 ${f U}$  : Flow variables at discrete grid points (implicit  ${f lpha}$  dep)

 $\mathbf{N}(\mathbf{U}, \boldsymbol{\alpha}) = 0$ : Discrete flow equations

#### Linearized form

• Linearize w.r.t  $\alpha$ 

$$\frac{dJ}{d\alpha} = \frac{\partial J}{\partial U}\frac{dU}{d\alpha} + \frac{\partial J}{\partial \alpha}$$

$$\text{s.t.} \quad \frac{\partial N}{\partial U}\frac{dU}{d\alpha} + \frac{\partial N}{\partial \alpha} = 0$$

• Defining  $\mathbf{u}:=rac{dU}{dlpha}$   $\mathbf{A}:=rac{\partial N}{\partial U}$   $\mathbf{f}:=-rac{\partial N}{\partial lpha}$   $\mathbf{h}^T:=rac{\partial J}{\partial U}$ , primal form is

$$\mathbf{h}^T \mathbf{u} + \frac{\partial J}{\partial \alpha}$$

 $\text{s.t.} \quad \mathbf{A}\mathbf{u} = \mathbf{f}(\alpha)$ 

## Discrete adjoint form

• The dual form is hence given by

$$\mathbf{f}^T \boldsymbol{\lambda} + \frac{\partial J}{\partial \alpha}$$
 s.t. 
$$\mathbf{A}^T \boldsymbol{\lambda} = \mathbf{h}$$

- $\mathbf{h}^T = \frac{\partial J}{\partial U}$  does not depend on design variables!
- Exploited in 2D and 3D aircraft wing optimization by Elliot and Peraire [1]

#### Lagrange Viewpoint

• Augmented objective function

$$I(U,\alpha) = J(U,\alpha) - \boldsymbol{\lambda}^T N(U,\alpha)$$

Linearizing it recovers the same dual form as earlier

$$\frac{dI}{d\alpha} = \frac{\partial J}{\partial \alpha} - \boldsymbol{\lambda}^T \frac{\partial N}{\partial \alpha} = \frac{\partial J}{\partial \alpha} + \mathbf{f}^T \boldsymbol{\lambda}$$

$$\left(\frac{\partial N}{\partial U}\right)^T \boldsymbol{\lambda} = \left(\frac{\partial J}{\partial U}\right)^T \Rightarrow \mathbf{A}^T \boldsymbol{\lambda} = \mathbf{h}$$

#### Continuous adjoint approach

$$< v, u>_{\Omega} := \int_{\Omega} v(x)u(x)dx$$

Primal

$$< h, u>_{\Omega}$$
 s.t.  $Lu=f$  HBC on  $\partial\Omega$ 

Dual

$$\label{eq:condition} \begin{split} &< v, f>_{\Omega}\\ \text{s.t.} \quad &L^*v=h\\ \text{HBC on } &\partial\Omega \end{split}$$

## Adjoint Operator

ullet For HBCs, the adjoint  $L^*$  of an operator L is defined by

$$\langle v, Lu \rangle = \langle L^*v, u \rangle$$

• Eg. If 
$$Lu = \left(\frac{d}{dx} - \epsilon \frac{d^2}{dx^2}\right)u, \quad 0 < x < 1, \quad u(0) = u(1) = 0$$

$$\langle v, Lu \rangle = \int_0^1 v \left( \frac{du}{dx} - \epsilon \frac{d^2u}{dx^2} \right) dx$$
$$= \int_0^1 u \left( -\frac{dv}{dx} - \epsilon \frac{d^2v}{dx^2} \right) + \left[ -\epsilon v \frac{du}{dx} \right]_0^1 = \langle L^*v, u \rangle$$

$$\Rightarrow L^* = \left(-\frac{d}{dx} - \epsilon \frac{d^2}{dx^2}\right) \quad v(0) = v(1) = 0$$

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# Green's function interpretation of the continuous adjoint approach

- $Lu = f \Rightarrow Lq_L(x, x') = \delta(x, x')$
- Given  $L^*v = h$ ,

$$\langle v, \delta(x, x') \rangle = \langle h, g(x, x') \rangle$$
  

$$\Rightarrow v(x) = \int_{\Omega} h(x')g_L(x, x')dx'$$

#### Generalized Adjoint Identity

If the primal objective includes a boundary integral, for eg

$$< h, u>_{\Omega} + < h_2, Cu>_{\partial\Omega}$$
 s.t.  $Lu = f$  in  $\Omega$  
$$Bu = f_2 \text{ on } \partial\Omega$$

• The adjoint identity is modified to

$$< v, Lu >_{\Omega} + < C^*v, Bu >_{\partial\Omega} = < L^*v, u >_{\Omega} + < B^*v, Cu >_{\partial\Omega}$$

This gives the dual form

$$< v, f>_{\Omega} + < C^*v, f_2>_{\partial\Omega}$$
 s.t.  $L^*v = h$  in  $\Omega$  
$$B^*v = h_2 \text{ on } \partial\Omega$$

# Main conceptual difference between the discrete and continuous approach

- Discrete approach : Discretize, Linearize, Adjoint
- Continuous approach : Linearize, Adjoint, Discretize

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#### Applications of the Adjoint method

- Aircraft design (eg. Optimal shape for drag and lift)
- Electromagnetic Shape Optimization (eg. Photonic components)

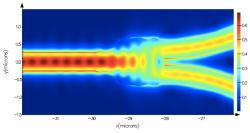


Fig. 5. Simulated field intensity  $|E|^2$  for the optimized structure at  $\lambda = 1550$ nm for a slice in the middle of the device.

Optimal Y-beam splitter, Lalau-Keraly et. al. [2]

#### **Authors**

• Giles and Pierce (2000) [3]



Michael Giles (Oxford)



Niles Pierce (Caltech)

(Images: Google)

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# Thank You

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